

8. Bearing Internal Clearance and Preload

8.1 Bearing internal clearance

Bearing internal clearance (initial clearance) is the amount of internal clearance a bearing has before being installed on a shaft or in a housing.

As shown in Fig. 8.1, when either the inner ring or the outer ring is fixed and the other ring is free to move, displacement can take place in either an axial or radial direction. This amount of displacement (radially or axially) is termed the internal clearance and, depending on the direction, is called the radial internal clearance or the axial internal clearance.

When the internal clearance of a bearing is measured, a slight measurement load is applied to the raceway so the internal clearance may be measured accurately. However, at this time, a slight amount of elastic deformation of the bearing occurs under the measurement load, and the clearance measurement value (measured clearance) is slightly larger than the true clearance. This discrepancy between the true bearing clearance and the increased amount due to the elastic deformation must be compensated for. These compensation values are given in Table 8.1. For roller bearings the amount of elastic deformation can be ignored.

The internal clearance values for each bearing class are shown in Tables 8.3 through 8.10.

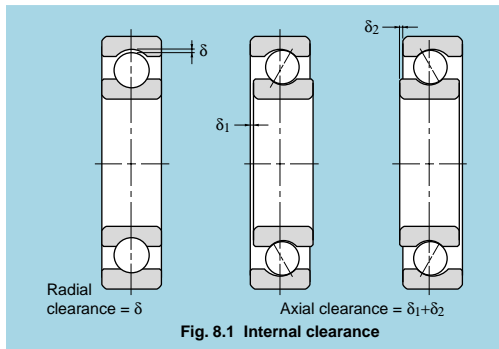


Table 8.1 Adjustment of radial internal clearance based on measured load Unit μm

Nominal Bore Diameter d (mm)	Measuring Load (N)	Radial Clearance Increase						
		over	incl.	C2	Normal	C3	C4	C5
10	18	24.5		3-4	4	4	4	4
18	50	49		4-5	5	6	6	6
50	200	147		6-8	8	9	9	9

8.2 Internal clearance selection

The internal clearance of a bearing under operating conditions (effective clearance) is usually smaller than the same bearing's initial clearance before being installed and operated. This is due to several factors including bearing fit, the difference in temperature between the inner and outer rings, etc. As a bearing's operating clearance has an effect on bearing life, heat generation, vibration, noise, etc.; care must be taken in selecting the most suitable operating clearance.

Effective internal clearance:

The initial clearance differential between the initial clearance and the operating (effective) clearance (the amount of clearance reduction caused by interference fits, or clearance variation due to the temperature difference between the inner and outer rings) can be calculated by the following formula:

$$\delta_{\text{eff}} = \delta_o - (\delta_f + \delta_t) \dots \dots \dots (8.1)$$

where,

- δ_{eff} : Effective internal clearance mm
- δ_o : Bearing internal clearance mm
- δ_f : Reduced amount of clearance due to interference mm
- δ_t : Reduced amount of clearance due to temperature differential of inner and outer rings mm

Reduced clearance due to interference:

When bearings are installed with interference fits on shafts and in housings, the inner ring will expand and the outer ring will contract; thus reducing the bearings' internal clearance. The amount of expansion or contraction varies depending on the shape of the bearing, the shape of the shaft or housing, dimensions of the respective parts, and the type of materials used. The differential can range from approximately 70% to 90% of the effective interference.

$$\delta_f = (0.70 \sim 0.90) \bullet \Delta_{\text{def}} \dots \dots \dots (8.2)$$

where,

- δ_t : Reduced amount of clearance due to interference mm
- Δ_{def} : Effective interference mm

Reduced internal clearance due to inner/outer ring temperature difference:

During operation, normally the outer ring will be from 5° to 10° cooler than the inner ring or rotating parts. However, if the cooling effect of the housing is large, the shaft is connected to a heat source, or a heated substance is conducted through the hollow shaft; the temperature difference between the two

rings can be even greater. The amount of internal clearance is thus further reduced by the differential expansion of the two rings.

$$\delta_i = \alpha \cdot \Delta_T \cdot D_o \dots\dots\dots(8.3)$$

where,

δ_i : Amount of reduced clearance due to heat differential mm

α : Bearing steel linear expansion coefficient $12.5 \times 10^{-6}/^\circ\text{C}$

Δ_T : Inner/outer ring temperature differential $^\circ\text{C}$

D_o : Outer ring raceway diameter mm

Outer ring raceway diameter, D_o , values can be approximated by using formula (8.4) or (8.5).

For ball bearings and self-aligning roller bearings,

$$D_o = 0.20(d + 4.0D) \dots\dots\dots(8.4)$$

For roller bearings (except self-aligning),

$$D_o = 0.25(d + 3.0D) \dots\dots\dots(8.5)$$

where,

d : Bearing bore diameter mm

D : Bearing outside diameter mm

8.3 Bearing internal clearance selection standards

Theoretically, to maximize life, the optimum operating internal clearance for any bearing would be a slight negative clearance after the bearing had reached normal operating temperature.

Unfortunately, under actual operating conditions, maintaining such optimum tolerances is often difficult at best. Due to various fluctuating operating conditions this slight negative clearance can quickly become a further negative, greatly lowering the life of the bearing and causing excessive heat to be generated. Therefore, an initial internal clearance which will result in a slightly greater than negative internal operating clearance should be selected.

Under normal operating conditions (e.g. normal load, fit, speed, temperature, etc.), a standard internal clearance will give a very satisfactory operating clearance.

Table 8.2 lists non-standard clearance recommendations for various applications and operating conditions.

Table 8.2 Examples of applications where bearing clearances other than normal clearances are used

Operating conditions	Applications	Selected clearance
With heavy or shock load, clearance is great.	Railway vehicle axles	C3
	Vibration screens	C3
With direction indeterminate load, both inner and outer rings are tight-fitted.	Railway vehicle traction motors	C4
	Tractors and final speed regulators	C4
Shaft or inner ring is heated.	Paper making machines and driers	C3, C4
	Rolling mill table rollers	C3
Clearance fit for both inner and outer rings.	Rolling mill roll necks	C2
To reduce noise and vibration when rotating.	Micromotors	C2
To reduce shaft runout, clearance is adjusted.	Main spindles of lathes (Double-row cylindrical roller bearings)	C9NA, C0NA

Table 8.3 Radial internal clearance of deep groove ball bearings

Unit μm

Nominal bore diameter d mm		C2		Normal		C3		C4		C5	
over	incl.	min	max	min	max	min	max	min	max	min	max
—	2.5	0	6	4	11	10	20	—	—	—	—
2.5	6	0	7	2	13	8	23	—	—	—	—
6	10	0	7	2	13	8	23	14	29	20	37
10	18	0	9	3	18	11	25	18	33	25	45
18	24	0	10	5	20	13	28	20	36	28	48
24	30	1	11	5	20	13	28	23	41	30	53
30	40	1	11	6	20	15	33	28	46	40	64
40	50	1	11	6	23	18	36	30	51	45	73
50	65	1	15	8	28	23	43	38	61	55	90
65	80	1	15	10	30	25	51	46	71	65	105
80	100	1	18	12	36	30	58	53	84	75	120
100	120	2	20	15	41	36	66	61	97	90	140
120	140	2	23	18	48	41	81	71	114	105	160
140	160	2	23	18	53	46	91	81	130	120	180
160	180	2	25	20	61	53	102	91	147	135	200
180	200	2	30	25	71	63	117	107	163	150	230
200	225	2	35	25	85	75	140	125	195	175	265
225	250	2	40	30	95	85	160	145	225	205	300
250	280	2	45	35	105	90	170	155	245	225	340
280	315	2	55	40	115	100	190	175	270	245	370
315	355	3	60	45	125	110	210	195	300	275	410
355	400	3	70	55	145	130	240	225	340	315	460
400	450	3	80	60	170	150	270	250	380	350	510
450	500	3	90	70	190	170	300	280	420	390	570
500	560	10	100	80	210	190	330	310	470	440	630
560	630	10	110	90	230	210	360	340	520	490	690
710	800	20	140	120	290	270	450	430	630	600	840
800	900	20	160	140	320	300	500	480	700	670	940
900	1000	20	170	150	350	330	550	530	770	740	1040
1000	1120	20	180	160	380	360	600	580	850	820	1150
1120	1250	20	190	170	410	390	650	630	920	890	1260

Table 8.5 Radial internal clearance of double row and duplex angular contact ball bearings

Unit μm

Nominal bore diameter d mm		C1		C2		Normal		C3		C4	
over	incl.	min	max	min	max	min	max	min	max	min	max
—	10	3	8	6	12	8	15	15	22	22	30
10	18	3	8	6	12	8	15	15	24	30	40
18	30	3	10	6	12	10	20	20	32	40	55
30	50	3	10	8	14	14	25	25	40	55	75
50	80	3	11	11	17	17	32	32	50	75	95
80	100	3	13	13	22	22	40	40	60	95	120
100	120	3	15	15	30	30	50	50	75	110	140
120	150	3	16	16	33	35	35	55	80	130	170
150	180	3	18	18	35	35	60	60	90	150	200
180	200	3	20	20	40	40	65	65	100	180	240

Note: The clearance group in the table is applied only to contact angles in the table below.

Contact angle symbol	Nominal contact angle	Applicable clearance group
C	15°	C1, C2
A ¹⁾	30°	C2, Normal, C3
B	40°	Normal, C3, C4

1) Usually not to be indicated

Table 8.6 Radial internal clearance of cylindrical roller bearings, needle roller bearings

Table 8.6 (1) Cylindrical Bore Interchangeable Radial Clearance ISO Cylindrical Roller Bearings ONLY

Unit μm

Nominal bore diameter d mm		C2		Normal		C3		C4		C5	
over	incl.	min	max	min	max	min	max	min	max	min	max
0	10	0	25	20	45	35	60	50	75	—	—
10	24	0	25	20	45	35	60	50	75	65	90
24	30	0	25	20	45	35	60	50	75	70	95
30	40	5	30	25	50	45	70	60	85	80	105
40	50	5	35	30	60	50	80	70	100	95	125
50	65	10	40	40	70	60	90	80	110	110	140
65	80	10	45	40	75	65	100	90	125	130	165
80	100	15	50	50	85	75	110	105	140	155	190
100	120	15	55	50	90	85	125	125	165	180	220
120	140	15	60	60	105	100	145	145	190	200	245
140	160	20	70	70	120	115	165	165	215	225	275
160	180	25	75	75	125	120	170	170	220	250	300
180	200	35	90	90	145	140	195	195	250	275	330
200	225	45	105	105	165	160	220	220	280	305	365
225	250	45	110	110	175	170	235	235	300	330	395
250	280	55	125	125	195	190	260	260	330	370	440
280	315	55	130	130	205	200	275	275	350	410	485
315	355	65	145	145	225	225	305	305	385	455	535
355	400	100	190	190	280	280	370	370	460	510	600
400	450	110	210	210	310	310	410	410	510	565	665
450	500	110	220	220	330	330	440	440	550	625	735
500	560	120	240	240	360	360	480	480	600	—	—
560	630	140	260	260	380	380	500	500	620	—	—
630	710	145	285	285	425	425	565	565	705	—	—
710	800	150	310	310	470	470	630	630	790	—	—
800	900	180	350	350	520	520	690	690	860	—	—
900	1000	200	390	390	580	580	770	770	960	—	—
1000	1120	220	430	430	640	640	850	850	1060	—	—
1120	1250	230	470	470	710	710	950	950	1190	—	—
1250	1400	270	530	530	790	790	1050	1050	1310	—	—

Table 8.6 (2) Tapered Bore Interchangeable Radial Clearance

Unit μm

Nominal bore diameter d mm		C2		Normal		C3		C4		C5	
over	incl.	min	max	min	max	min	max	min	max	min	max
0	24	15	40	30	55	40	65	50	75	—	—
24	30	20	45	35	60	45	70	55	80	—	—
30	40	20	45	40	65	55	80	70	95	—	—
40	50	25	55	45	75	60	90	75	105	—	—
50	65	30	60	50	80	70	100	90	120	—	—
65	80	35	70	60	95	85	120	110	145	—	—
80	100	40	75	70	105	95	130	120	155	—	—
100	120	50	90	90	130	115	155	140	180	—	—
120	140	55	100	100	145	130	175	160	205	—	—
140	160	60	110	110	160	145	195	180	230	—	—
160	180	75	125	125	175	160	210	195	245	—	—
180	200	85	140	140	195	180	235	220	275	—	—
200	225	95	155	155	215	200	260	245	305	—	—
225	250	105	170	170	235	220	285	270	335	—	—
250	280	115	185	185	255	240	310	295	365	—	—
280	315	130	205	205	280	265	340	325	400	—	—
315	355	145	225	225	305	290	370	355	435	—	—
355	400	165	225	255	345	330	420	405	495	—	—
400	450	185	285	285	385	370	470	455	555	—	—
450	500	205	315	315	425	410	520	505	615	—	—

Table 8.7 Radial internal clearance of cylindrical roller bearings, needle roller bearings (Non-interchangeable)

Nominal bore diameter d mm		Bearing with cylindrical bore											
		C1NA		C2NA		NA ¹⁾		C3NA		C4NA		C5NA	
over	incl.	min	max	min	max	min	max	min	max	min	max	min	max
—	10	5	10	10	20	20	30	35	45	45	55	—	—
10	18	5	10	10	20	20	30	35	45	45	55	65	75
18	24	5	10	10	20	20	30	35	45	45	55	65	75
24	30	5	10	10	25	25	35	40	50	50	60	70	80
30	40	5	12	12	25	25	40	45	55	55	70	80	95
40	50	5	15	15	30	30	45	50	65	65	80	95	110
50	65	5	15	15	35	35	50	55	75	75	90	110	130
65	80	10	20	20	40	40	60	70	90	90	110	130	150
80	100	10	25	25	45	45	70	80	105	105	125	155	180
100	120	10	25	25	50	50	80	95	120	120	145	180	205
120	140	15	30	30	60	60	90	105	135	135	160	200	230
140	160	15	35	35	65	65	100	115	150	150	180	225	260
160	180	15	35	35	75	75	110	125	165	165	200	250	285
180	200	20	40	40	80	80	120	140	180	180	220	275	315
200	225	20	45	45	90	90	135	155	200	200	240	305	350
225	250	25	50	50	100	100	150	170	215	215	265	330	380
250	280	25	55	55	110	110	165	185	240	240	295	370	420
280	315	30	60	60	120	120	180	205	265	265	325	410	470
315	355	30	65	65	135	135	200	225	295	295	360	455	520
355	400	35	75	75	150	150	225	255	330	330	405	510	585
400	450	45	85	85	170	170	255	285	370	370	455	565	650
450	500	50	95	95	190	190	285	315	410	410	505	625	720

1) For bearings with normal clearance, only NA is added to bearing numbers. Ex. NU310NA, NN03020KNAP5

Table 8.4 Radial internal clearance of self-aligning ball bearings

Nominal bore diameter d mm		Bearing with cylindrical bore									
		C2		Normal		C3		C4		C5	
over	incl.	min	max	min	max	min	max	min	max	min	max
2.5	6	1	8	5	15	10	20	15	25	21	33
6	10	2	9	6	17	12	25	19	33	27	42
10	14	2	10	6	19	13	26	21	35	30	48
14	18	3	12	8	21	15	28	23	37	32	50
18	24	4	14	10	23	17	30	25	39	34	52
24	30	5	16	11	24	19	35	29	46	40	58
30	40	6	18	13	29	23	40	34	53	46	66
40	50	6	19	14	31	25	44	37	57	50	71
50	65	7	21	16	36	30	50	45	69	62	88
65	80	8	24	18	40	35	60	54	83	76	108
80	100	9	27	22	48	42	70	64	96	89	124
100	120	10	31	25	56	50	83	75	114	105	145
120	140	10	38	30	68	60	100	90	135	125	175
140	160	15	44	35	80	70	120	110	161	150	210

Table 8.7 (Cont.) Radial internal clearance of cylindrical roller bearings, needle roller bearings (Non-interchangeable bore) μm

Bearing with tapered bore												Nominal bore diameter d mm	
C9NA		C0NA ²⁾		C1NA ²⁾		C2NA		NA ¹⁾		C3NA		over	incl.
min	max	min	max	min	max	min	max	min	max	min	max		
5	5	7	17	10	20	20	30	35	45	45	55	—	10
5	10	7	17	10	20	20	30	35	45	45	55	10	18
5	10	7	17	10	20	20	30	35	45	45	55	18	24
5	10	10	20	10	25	25	35	40	50	50	60	24	30
5	12	10	20	12	25	25	40	45	55	55	70	30	40
5	15	10	20	15	30	30	45	50	65	65	80	40	50
5	15	10	20	15	35	35	50	55	75	75	90	50	65
10	20	15	30	20	40	40	60	70	90	90	110	65	80
10	25	20	35	25	45	45	70	80	105	105	125	80	100
10	25	20	35	25	50	50	80	95	120	120	145	100	120
15	30	25	40	30	60	60	90	105	135	135	160	120	140
15	35	30	45	35	65	65	100	115	150	150	180	140	160
15	35	30	45	35	75	75	110	125	165	165	200	160	180
20	40	30	50	40	80	80	120	140	180	180	220	180	220
20	45	35	55	45	90	90	135	155	200	200	240	200	225
25	50	40	65	50	100	100	150	170	215	215	265	225	250
25	55	40	65	55	110	110	165	185	240	240	295	250	280
30	60	45	75	60	120	120	180	205	265	265	325	280	315
30	65	45	75	65	135	135	200	225	295	295	360	315	355
35	75	50	90	75	150	150	225	255	330	330	405	355	400
45	85	60	100	85	170	170	255	285	370	370	455	400	450
50	95	70	115	95	190	190	285	315	410	410	505	450	500

2) C9NA, C0NA and C1NA are applied only to precision bearings of class 5 and higher.

Unit μm

Bearing with tapered bore										Nominal bore diameter d mm	
C2		Normal		C3		C4		C5		over	incl.
min	max	min	max	min	max	min	max	min	max		
—	—	—	—	—	—	—	—	—	—	2.5	6
—	—	—	—	—	—	—	—	—	—	6	10
—	—	—	—	—	—	—	—	—	—	10	14
—	—	—	—	—	—	—	—	—	—	14	18
7	17	13	26	20	33	28	42	37	55	18	24
9	20	15	28	23	39	33	50	44	62	24	30
12	24	19	35	29	46	40	59	52	72	30	40
14	27	22	39	33	52	45	65	58	79	40	50
18	32	27	47	41	61	56	80	73	99	50	65
23	39	35	57	50	75	69	98	91	123	65	80
29	47	42	68	62	90	84	116	109	144	80	100
35	56	50	81	75	108	100	139	130	170	100	120
40	68	60	98	90	130	120	165	155	205	120	140
45	74	65	110	100	150	140	191	180	240	140	160

Table 8.8 Axial internal clearance of metric double row and duplex tapered roller bearings

(Except series 329X, 322C, 323C)

Nominal bore diameter d mm		Contact angle $\alpha \leq 27^\circ$ ($e \leq 0.76$)							
		C2		Normal		C3		C4	
over	incl.	min	max	min	max	min	max	min	max
18	24	25	75	75	125	125	170	170	220
24	30	25	75	75	125	145	195	195	245
30	40	25	95	95	165	165	235	210	280
40	50	20	85	85	150	175	240	240	305
50	65	20	85	110	175	195	260	280	350
65	80	20	110	130	220	240	325	325	410
80	100	45	150	150	260	280	390	390	500
100	120	45	175	175	305	350	480	455	585
120	140	45	175	175	305	390	520	500	630
140	160	60	200	200	340	400	540	520	660
160	180	80	220	240	380	440	580	600	740
180	200	100	260	260	420	500	660	660	820
200	225	120	300	300	480	560	740	720	900
225	250	160	360	360	560	620	820	820	1020
250	280	180	400	400	620	700	920	920	1140
280	315	200	440	440	680	780	1020	1020	1260
315	355	220	480	500	760	860	1120	1120	1380
355	400	260	560	560	860	980	1280	1280	1580
400	500	300	600	620	920	1100	1400	1440	1740

Note: Radial internal clearance is approximately obtained from:

$$\Delta r = \frac{e}{1.5} \Delta_a$$

where Δr = radial internal clearance, μm
 Δ_a = axial internal clearance, μm
 e = constant, see bearing tables

Table 8.8 (Cont.) Axial internal clearance of metric double row and duplex tapered roller bearings

(Except series 329X, 322CUB, 320)

Contact angle $\alpha > 27^\circ$ ($\epsilon > 0.76$)								Nominal bore diameter d mm	
C2		Normal		C3		C4			
min	max	min	max	min	max	min	max	over	incl.
10	30	30	50	50	70	70	90	18	24
10	30	30	50	60	80	80	100	24	30
10	40	40	70	70	100	90	120	30	40
10	40	40	70	80	110	110	140	40	50
10	40	50	80	90	120	130	160	50	65
10	50	60	100	110	150	150	190	65	80
20	70	70	120	130	180	180	230	80	100
20	70	70	120	150	200	210	260	100	120
20	70	70	120	160	210	210	260	120	140
30	100	100	160	180	240	240	300	140	160
—	—	—	—	—	—	—	—	160	180
—	—	—	—	—	—	—	—	180	200
—	—	—	—	—	—	—	—	200	225
—	—	—	—	—	—	—	—	225	250
—	—	—	—	—	—	—	—	250	280
—	—	—	—	—	—	—	—	280	315
—	—	—	—	—	—	—	—	315	355
—	—	—	—	—	—	—	—	355	400
—	—	—	—	—	—	—	—	400	500

Table 8.10 Radial internal clearance of bearings for electric motor

Unit μm

Nominal bore diameter d mm		Radial internal clearance $CM^{1)}$			
		Deep groove ball bearings		Cylindrical ²⁾ roller bearings	
over	incl.	min	max	min	max
10 ³⁾	18	4	11	—	—
18	24	5	12	—	—
24	30	5	12	15	30
30	40	9	17	15	30
40	50	9	17	20	35
50	65	12	22	25	40
65	80	12	22	30	45
80	100	18	30	35	55
100	120	18	30	35	60
120	140	24	38	40	65
140	160	24	38	50	80
160	180	—	—	60	90
180	200	—	—	65	100

1) Suffix CM is added to bearing numbers.

2) Non-interchangeable clearance.

3) This diameter is included in the group.

Table 8.9 Radial internal clearance of spherical roller bearings

Nominal bore diameter d mm		Bearing with cylindrical bore									
		C2		Normal		C3		C4		C5	
over	incl.	min	max	min	max	min	max	min	max	min	max
14	18	10	20	20	35	35	45	45	60	60	75
18	24	10	20	20	35	35	45	45	60	60	75
24	30	15	25	25	40	40	55	55	75	75	95
30	40	15	30	30	45	45	60	60	80	80	100
40	50	20	35	35	55	55	75	75	100	100	125
50	65	20	40	40	65	65	90	90	120	120	150
65	80	30	50	50	80	80	110	110	145	145	180
80	100	35	60	60	100	100	135	135	180	180	225
100	120	40	75	75	120	120	160	160	210	210	260
120	140	50	95	95	145	145	190	190	240	240	300
140	160	60	110	110	170	170	220	220	280	280	350
160	180	65	120	120	180	180	240	240	310	310	390
180	200	70	130	130	200	200	260	260	340	340	430
200	225	80	140	140	220	220	290	290	380	380	470
225	250	90	150	150	240	240	320	320	420	420	520
250	280	100	170	170	260	260	350	350	460	460	570
280	315	110	190	190	280	280	370	370	500	500	630
315	355	120	200	200	310	310	410	410	550	550	690
355	400	130	220	220	340	340	450	450	600	600	750
400	450	140	240	240	370	370	500	500	660	660	820
450	500	140	260	260	410	410	550	550	720	720	900
500	560	150	280	280	440	440	600	600	780	780	1000
560	630	170	310	310	480	480	650	650	850	850	1100
630	710	190	350	350	530	530	700	700	920	920	1190
710	800	210	390	390	580	580	770	770	1010	1010	1300
800	900	230	430	430	650	650	860	860	1120	1120	1440
900	1000	260	480	480	710	710	930	930	1220	1220	1570
1000	1120	290	530	530	780	780	1020	1020	1330	1330	1720
1120	1250	320	580	280	860	860	1120	1120	1460	1460	1870
1250	1400	350	640	640	950	950	1240	1240	1620	1620	2080

Table 8.9 (Cont.) Radial internal clearance of spherical roller bearings

Unit μm

Bearing with tapered bore										Nominal bore diameter d mm	
C2		Normal		C3		C4		C5		over	incl.
min	max	min	max	min	max	min	max	min	max		
—	—	—	—	—	—	—	—	—	—	14	18
15	25	25	35	35	45	45	60	60	75	18	24
20	30	30	40	40	55	55	75	75	95	24	30
25	35	35	50	50	65	65	85	85	105	30	40
30	45	45	60	60	80	80	100	100	130	40	50
40	55	55	75	75	95	95	120	120	160	50	65
50	70	70	95	95	120	120	150	150	200	65	80
55	80	80	110	110	140	140	180	180	230	80	100
65	100	100	135	135	170	170	220	220	280	100	120
80	120	120	160	160	200	200	260	260	330	120	140
90	130	130	180	180	230	230	300	300	380	140	160
100	140	140	200	200	260	260	340	340	430	160	180
110	160	160	220	220	290	290	370	370	470	180	200
120	180	180	250	250	320	320	410	410	520	200	225
140	200	200	270	270	350	350	450	450	570	225	250
150	220	220	300	300	390	390	490	490	620	250	280
170	240	240	330	330	430	430	540	540	680	280	315
190	270	270	360	360	470	470	590	590	740	315	355
210	300	300	400	400	520	520	650	650	820	355	400
230	330	330	440	440	570	570	720	720	910	400	450
260	370	370	490	490	630	630	790	790	1000	450	500
290	410	410	540	540	680	680	870	870	1100	500	560
320	460	460	600	600	760	760	980	980	1230	560	630
350	510	510	670	670	850	850	1090	1090	1360	630	710
390	570	570	750	750	960	960	1220	1220	1500	710	800
440	640	640	840	840	1070	1070	1370	1370	1690	800	900
490	710	710	930	930	1190	1190	1520	1520	1860	900	1000
530	770	770	1030	1030	1300	1300	1670	1670	2050	1000	1120
570	830	830	1120	1120	1420	1420	1830	1830	2250	1120	1250
620	910	910	1230	1230	1560	1560	2000	2000	2470	1250	1400

8.4 Preload

Normally, bearings are used with a slight internal clearance under operating conditions. However, in some applications, bearings are given an initial load; this means that the bearings' internal clearance is negative before operation. This is called "preload" and is commonly applied to angular ball bearings and tapered roller bearings.

8.4.1 Purpose of preload

Giving preload to a bearing results in the rolling element and raceway surfaces being under constant elastic compressive forces at their contact points. This has the effect of making the bearing extremely rigid so that even when load is applied to the bearing, radial or axial shaft displacement does not occur. Thus, the natural frequency of the shaft is increased, which is suitable for high speeds.

Preload is also used to prevent or suppress shaft runout, vibration, and noise; improve running accuracy and locating accuracy; reduce smearing, and regulate rolling element rotation. Also, for thrust ball and roller bearings mounted on horizontal shafts, preloading keeps the rolling elements in proper alignment.

The most common method of preloading is to apply an axial load to two duplex bearings so that the inner and outer rings are displaced axially in relation to each other. This preloading method is divided into fixed position preload and constant pressure preload.

8.4.2 Preloading methods and amounts

The basic pattern, purpose and characteristics of bearing preloads are shown in Table 8.11. The definite position preload is effective for positioning the two bearings and also for increasing the rigidity. Due to the use of a spring for the constant pressure preload, the preload force can be kept constant, even when the distance between the two bearings fluctuates under the influence of operating heat and load.

Also, the standard preload for the paired angular contact ball bearings is shown in Table 8.12. Light and normal preload is applied to prevent general vibration, and medium and heavy preload is applied especially when rigidity is required.

8.4.3 Preload and rigidity

The increased rigidity effect preloading has on bearings is shown in Fig. 8.5. When the offset inner rings of the two paired angular contact ball bearings are pressed together, each inner ring is displaced axially by the amount δ_o and is thus given a preload, F_o , in the direction shown. Under this condition, when external axial load F_a is applied, bearing I will have an increased displacement by the amount δ_a and bearing II's displacement will decrease. At this time the loads applied to bearing I and II are F_I and F_{II} respectively.

Under the condition of no preload, bearing I will be displaced by the amount δ_b when axial load F_a is applied. Since the amount of displacement, δ_a , is less than δ_b , it indicates a higher rigidity for δ_a .

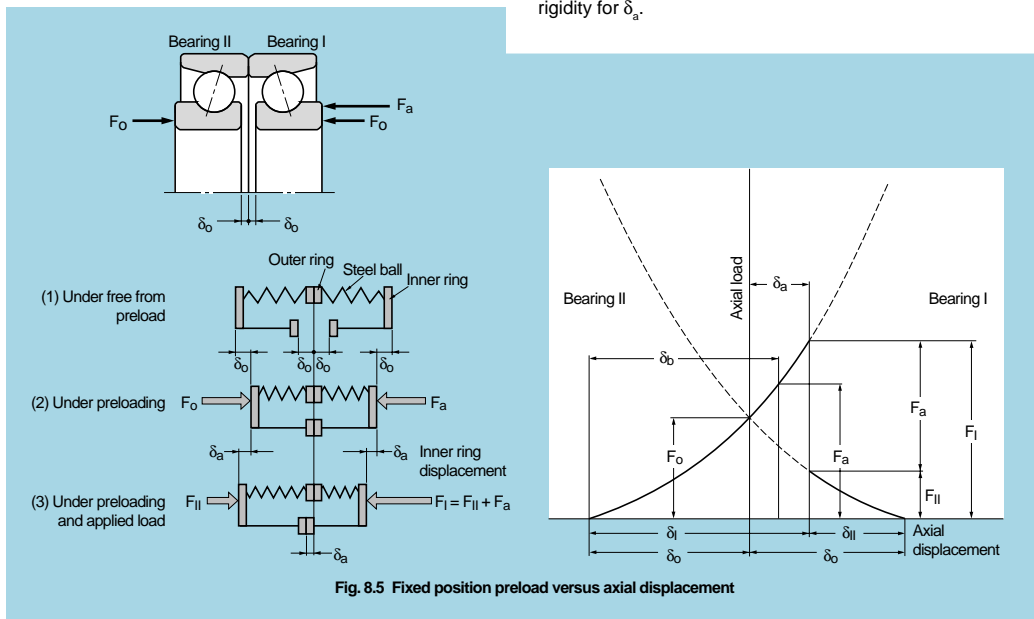
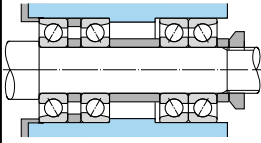
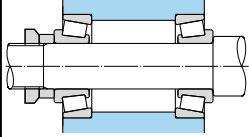
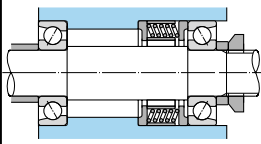
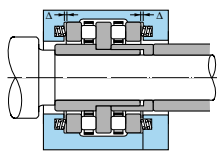


Table 8.11 Preloading methods and characteristics

Method	Basic pattern	Applicable bearings	Object	Characteristics	Applications
Fixed position preload		Precision angular contact ball bearings	Maintaining accuracy of rotating shaft, preventing vibration increasing rigidity	Preload is accomplished by a predetermined offset of the rings or by using spacers. For the standard preload see Table 8.12	Grinding machines, lathes, milling machines, measuring instruments
		Tapered roller bearings, thrust ball bearings, angular contact ball bearings	Increasing bearing rigidity	Preload is accomplished by adjusting a threaded screw. The amount of preload is set by measuring the starting torque or axial displacement. Relationship between the starting torque M and preload T is approximately given by the following formulas: for duplex angular contact ball bearings:	Lathes, milling machines, differential gears of automobiles, printing machines, wheel axles
Constant pressure preload		Angular contact ball bearings, deep groove ball bearings, precision tapered roller bearings	Maintaining accuracy and preventing vibration and noise with a constant amount of preload without being affected by loads or temperature	Preloading is accomplished by using coil or Belleville springs. Recommended preloads are as follows: for deep groove ball bearings: $(4 \text{ to } 8) d \cdot N$ for angular contact ball bearings: see Table 8.12	Internal grinding machines, electric motors, high speed shafts in small machines, tension reels
		Tapered roller bearings with steep angle, spherical roller thrust bearings, thrust ball bearings	Preventing smearing on raceway of non-loaded side under axial loads	Preload is accomplished by using coil or Belleville springs. Recommended preloads are as follows: for thrust ball bearings: $T = 0.42(n \cdot C_{0a})^{1.9} \times 10^{-13} \text{ N}^2$ $T = 0.00083 C_{0a} \text{ N}^2$ whichever is greater for spherical roller thrust bearings: $T = 0.025 C_{0a}^{0.8} \text{ N}^2$	Rolling mills, extruding machines

Note: In the above formulas,

d_p = pitch diameter of bearing, mm
 $d_p = (\text{Bore} + \text{Outside dia}) / 2$
 T = preload, N

d = bearing bore, mm
 n = number of revolutions, r/min
 C_{0a} = basic static axial load rating, N

The starting torque M however, is greatly influenced by lubricants and a period of run-in time.

Table 8.12 Standard preloads for angular contact ball bearings

Units: (N)

Nominal bore diameter		Bearing series															
d mm		78C				79C, HSB9C				70C, BNT0, HSB0C				72C, BNT2			
over	incl.	Light	Normal	Medium	Heavy	Light	Normal	Medium	Heavy	Light	Normal	Medium	Heavy	Light	Normal	Medium	Heavy
—	12	—	—	—	—	—	—	—	—	20	30	100	150	20	50	100	200
12	18	—	—	—	—	—	—	—	—	20	30	100	200	20	50	150	300
18	32	10	30	80	150	20	50	100	200	30	80	150	300	50	100	300	500
32	40	10	30	80	150	30	80	200	300	50	150	300	600	80	200	500	800
40	50	20	50	100	200	40	100	250	500	50	150	300	700	100	300	600	1000
50	65	30	100	200	400	50	120	300	600	100	200	500	1000	150	400	800	1500
65	80	30	100	200	400	80	200	400	800	100	300	700	1500	200	500	1000	2000
80	90	50	150	300	600	100	250	500	1000	150	400	1000	2000	300	700	1500	3000
90	95	50	150	300	600	100	250	500	1000	150	400	1000	2000	300	700	2000	4000
95	100	50	150	300	600	120	300	700	1500	150	400	1000	2000	300	700	2000	4000
100	105	50	150	300	600	120	300	700	1500	200	600	1500	2500	400	1000	2500	5000
105	110	80	200	500	1000	120	300	700	1500	200	600	1500	2500	400	1000	2500	5000
110	120	80	200	500	1000	150	400	900	2000	200	600	1500	2500	400	1000	2500	5000
120	140	100	300	600	1300	200	500	1000	2500	300	800	2000	4000	500	1500	3000	6000
140	150	150	400	800	1500	250	700	1500	3000	300	800	2000	4000	500	1500	3000	6000
150	160	150	400	800	1500	250	700	1500	3000	500	1000	2500	6000	700	2000	4500	8000
160	170	150	500	1000	2000	250	700	1500	3000	500	1000	2500	6000	700	2000	4500	8000
170	180	150	500	1000	2000	300	900	2000	4000	500	1000	2500	6000	700	2000	4500	8000
180	190	200	600	1300	2500	300	900	2000	4000	600	1500	3500	7000	800	2500	5000	10000
190	200	200	600	1300	2500	500	1300	3000	6000	600	1500	3500	7000	800	2500	5000	10000

Note: Symbols /GL, /GN, /GM and GH are suffixes on NTN bearing part numbers indicating Light, Normal, Medium and Heavy preloads, respectively.